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机器人学

人工智能学院 杨智勇
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刚体的加速度

► 速度矢量 V_Q 的微分

$${}^B A_Q = \frac{d}{dt} {}^B V_Q = \lim_{\Delta t \rightarrow 0} \frac{{}^B V_Q(t + \Delta t) - {}^B V_Q(t)}{\Delta t}$$

速度矢量 ${}^B V_Q$ 相对于坐标系 {B} 的微分



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$${}^A ({}^B A_Q) = {}^A \left(\frac{d}{dt} {}^B V_Q \right)$$

在坐标系 {A} 的表达



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在坐标系 {A} 的表达

$$= \underline{{}^A_B R} \underline{{}^B A_Q} = \underline{{}^A_B R} \underline{{}^B A_Q} \quad \text{两个坐标系相同时的表达}$$



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$$a_C = {}^U A_C \text{ ORG}$$

坐标系 {C} 的原点相对于世界参考坐标系的加速度



刚体的加速度

► 角加速度矢量 ${}^A\dot{\Omega}_B$

$${}^A\dot{\Omega}_B = \frac{d}{dt} {}^A\Omega_B = \lim_{\Delta t \rightarrow 0} \frac{{}^A\Omega_B(t + \Delta t) - {}^A\Omega_B(t)}{\Delta t}$$

坐标系 {B} 相对于坐标系 {A} 的角速度的微分



刚体的加速度

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$${}^A\dot{\Omega}_B = \frac{d}{dt} {}^A\Omega_B = \lim_{\Delta t \rightarrow 0} \frac{{}^A\Omega_B(t + \Delta t) - {}^A\Omega_B(t)}{\Delta t}$$

坐标系 {B} 相对于坐标系 {A} 的角速度的微分

$${}^C({}^A\dot{\Omega}_B)$$

在坐标系 {C} 中的表达



刚体的加速度

► 角加速度矢量 ${}^A\dot{\Omega}_B$

$${}^A\dot{\Omega}_B = \frac{d}{dt} {}^A\Omega_B = \lim_{\Delta t \rightarrow 0} \frac{{}^A\Omega_B(t + \Delta t) - {}^A\Omega_B(t)}{\Delta t}$$

坐标系 {B} 相对于坐标系 {A} 的角速度的微分

$${}^C({}^A\dot{\Omega}_B)$$

在坐标系 {C} 中的表达

$$\dot{\omega}_C = {}^U\dot{\Omega}_C$$

坐标系 {C} 相对于世界参考坐标系 {U} 的角加速度



刚体的加速度

► 角加速度

$${}^A\Omega_C = {}^A\Omega_B + {}^A_B R {}^B\Omega_C$$



刚体的加速度

► 角加速度

$${}^A\Omega_C = {}^A\Omega_B + {}^A_B R {}^B\Omega_C$$

↓ diff.

$$\begin{aligned} {}^A\dot{\Omega}_C &= {}^A\dot{\Omega}_B + \frac{d}{dt} {}^A_B R {}^B\Omega_C \\ &= {}^A\dot{\Omega}_B + {}^A_B R {}^B\dot{\Omega}_C + {}^A\Omega_B \times {}^A_B R {}^B\Omega_C \end{aligned}$$



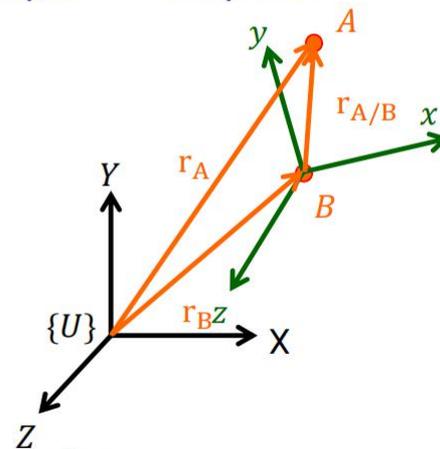
刚体的运动

► 动态运动

根据第5章的描述

$$\vec{v}_A = \vec{v}_B + \vec{v}_{rel} + \vec{\omega} \times \vec{r}_{A/B}$$

$$\vec{v}_A = (\dot{x}_B \hat{I} + \dot{y}_B \hat{J}) + (\dot{x}_{A/B} \hat{i} + \dot{y}_{A/B} \hat{j}) + \vec{\omega} \times (x_{A/B} \hat{i} + y_{A/B} \hat{j})$$





刚体的运动

► 动态运动

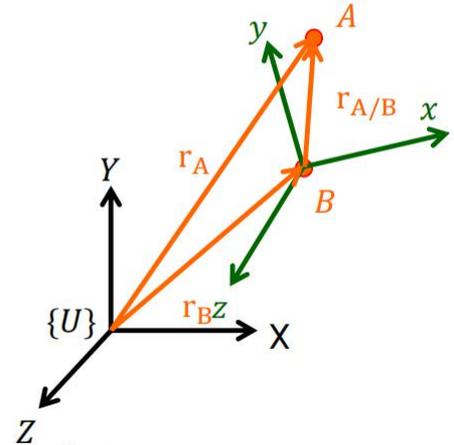
根据第5章的描述

$$\vec{v}_A = \vec{v}_B + \vec{v}_{rel} + \vec{\omega} \times \vec{r}_{A/B}$$

$$\vec{v}_A = (\dot{x}_B \hat{I} + \dot{y}_B \hat{J}) + (\dot{x}_{A/B} \hat{i} + \dot{y}_{A/B} \hat{j}) + \vec{\omega} \times (x_{A/B} \hat{I} + y_{A/B} \hat{J})$$

↓ diff.

$$\begin{aligned} \vec{a}_A = & (\ddot{x}_B \hat{I} + \ddot{y}_B \hat{J}) \\ & + (\ddot{x}_{A/B} \hat{i} + \ddot{y}_{A/B} \hat{j}) + \vec{\omega} \times (\dot{x}_{A/B} \hat{i} + \dot{y}_{A/B} \hat{j}) \\ & + \dot{\vec{\omega}} \times (x_{A/B} \hat{I} + y_{A/B} \hat{J}) \\ & + \vec{\omega} \times ((\dot{x}_{A/B} \hat{i} + \dot{y}_{A/B} \hat{j}) + \vec{\omega} \times (x_{A/B} \hat{I} + y_{A/B} \hat{J})) \end{aligned}$$





刚体的运动

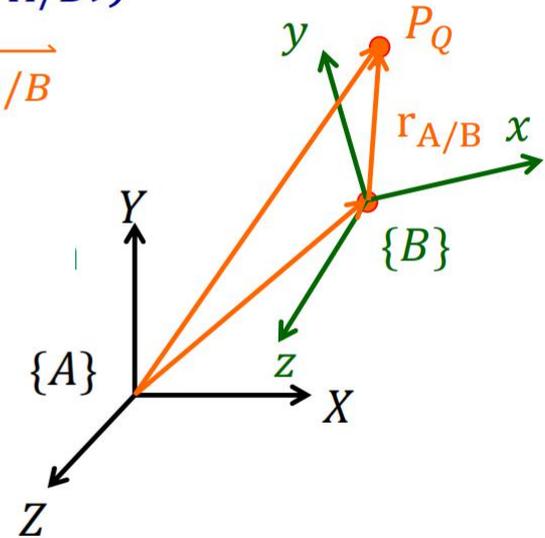
$$\begin{aligned} \vec{a}_A &= (\ddot{x}_B \hat{I} + \ddot{y}_B \hat{J}) \\ &+ \dot{\vec{\omega}} \times (x_{A/B} \hat{I} + y_{A/B} \hat{J}) + \vec{\omega} \times (\vec{\omega} \times (x_{A/B} \hat{I} + y_{A/B} \hat{J})) \\ &+ 2\vec{\omega} \times (\dot{x}_{A/B} \hat{I} + \dot{y}_{A/B} \hat{J}) + (\ddot{x}_{A/B} \hat{I} + \ddot{y}_{A/B} \hat{J}) \end{aligned}$$

$$\begin{aligned} \vec{a}_A &= \vec{a}_B + \dot{\vec{\omega}} \times \vec{r}_{A/B} + \vec{\omega} \times \vec{\omega} \times \vec{r}_{A/B} \\ &+ \underbrace{2\vec{\omega} \times \vec{v}_{rel}}_{\text{科氏加速度}} + \underbrace{\vec{a}_{rel}}_{\text{相对加速度}} \end{aligned}$$

科氏加速度 相对加速度

➤ 因此

$$\begin{aligned} {}^A A_Q &= {}^A A_B \text{ ORG} \\ &+ {}^A \dot{\Omega}_B \times {}^A R^B P_Q + {}^A \Omega_B \times ({}^A \Omega_B \times {}^A R^B P_Q) \\ &+ 2 {}^A \Omega_B \times {}^A R^B V_Q + {}^A R^B A_Q \end{aligned}$$

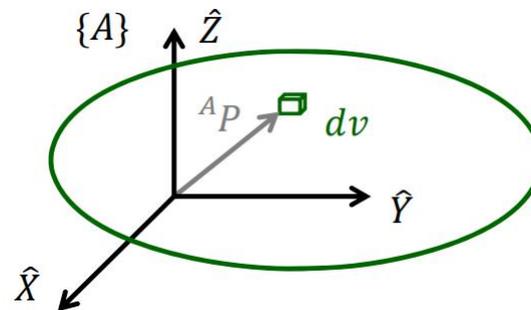




质量分布

► 相对于坐标系 {A} 的惯性张量

$${}^A I = \begin{bmatrix} I_{xx} & -I_{xy} & -I_{xz} \\ -I_{xy} & I_{yy} & -I_{yz} \\ -I_{xz} & -I_{yz} & I_{zz} \end{bmatrix}$$



惯性矩

$$I_{xx} = \iiint_V (y^2 + z^2) \rho dv$$

$$I_{yy} = \iiint_V (x^2 + z^2) \rho dv$$

$$I_{zz} = \iiint_V (x^2 + y^2) \rho dv$$

惯性积

$$I_{xy} = \iiint_V xy \rho dv$$

$$I_{xz} = \iiint_V xz \rho dv$$

$$I_{yz} = \iiint_V yz \rho dv$$



质量分布

➤ 惯性张量

◆ 实常数对称矩阵（可以正交对角化）

它的特征分解（也就是 $M = V\Lambda V^{-1}$ ）

$${}^A I = \begin{bmatrix} I_{xx} & -I_{xy} & -I_{xz} \\ -I_{xy} & I_{yy} & -I_{yz} \\ -I_{xz} & -I_{yz} & I_{zz} \end{bmatrix} = R \begin{bmatrix} I_{XX} & 0 & 0 \\ 0 & I_{YY} & 0 \\ 0 & 0 & I_{ZZ} \end{bmatrix} R^T$$

主惯性矩

旋转矩阵，揭示了
主轴的方向

◆ $I_{xx} + I_{yy} + I_{zz} = \text{trace}({}^A I) = \text{constant}$

● 迹在相似变换下是不变的

◆ 如果xy平面是对称平面，则 $I_{xz} = I_{yz} = 0$



➤ 平行轴原理

◆ 计算惯性张量在参考坐标系平移下的变化

$${}^A I_{zz} = {}^C I_{zz} + m(x_c^2 + y_c^2)$$

$${}^A I_{xy} = {}^C I_{xy} - mx_c y_c$$

C: 刚体的重心 (COM)

A: 任意坐标系

◆ 矩阵向量形式

$${}^A I = {}^C I + m[P_c^T P_c I_3 - P_c P_c^T]$$

$$P_c = [x_c \quad y_c \quad z_c]^T$$

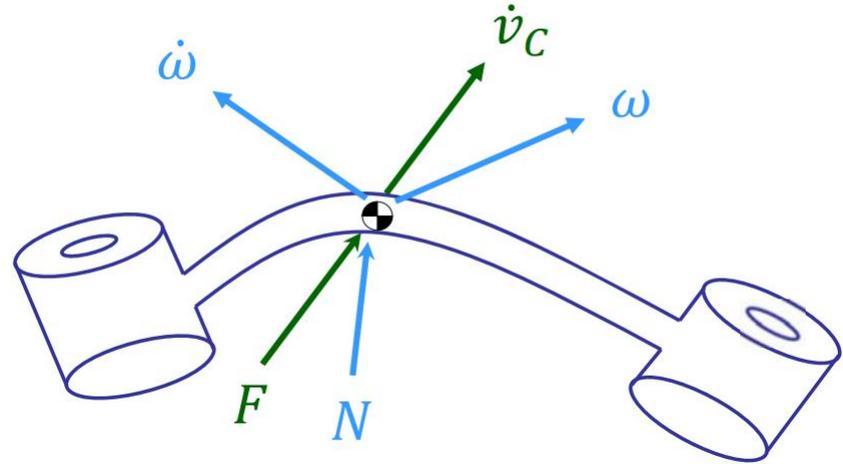
相对于坐标系 {A} 的COM



牛顿方程和欧拉方程

➤ 牛顿方程

$$F = \frac{d}{dt}(mv_C) = m\dot{v}_C$$



➤ 欧拉方程

$$N = \frac{d}{dt}(\underline{I}\omega)$$

即使使用惯性坐标系，它在运动过程中也可能变化

$$N = \underline{C}I\dot{\omega} + \omega \times \underline{C}I\omega$$

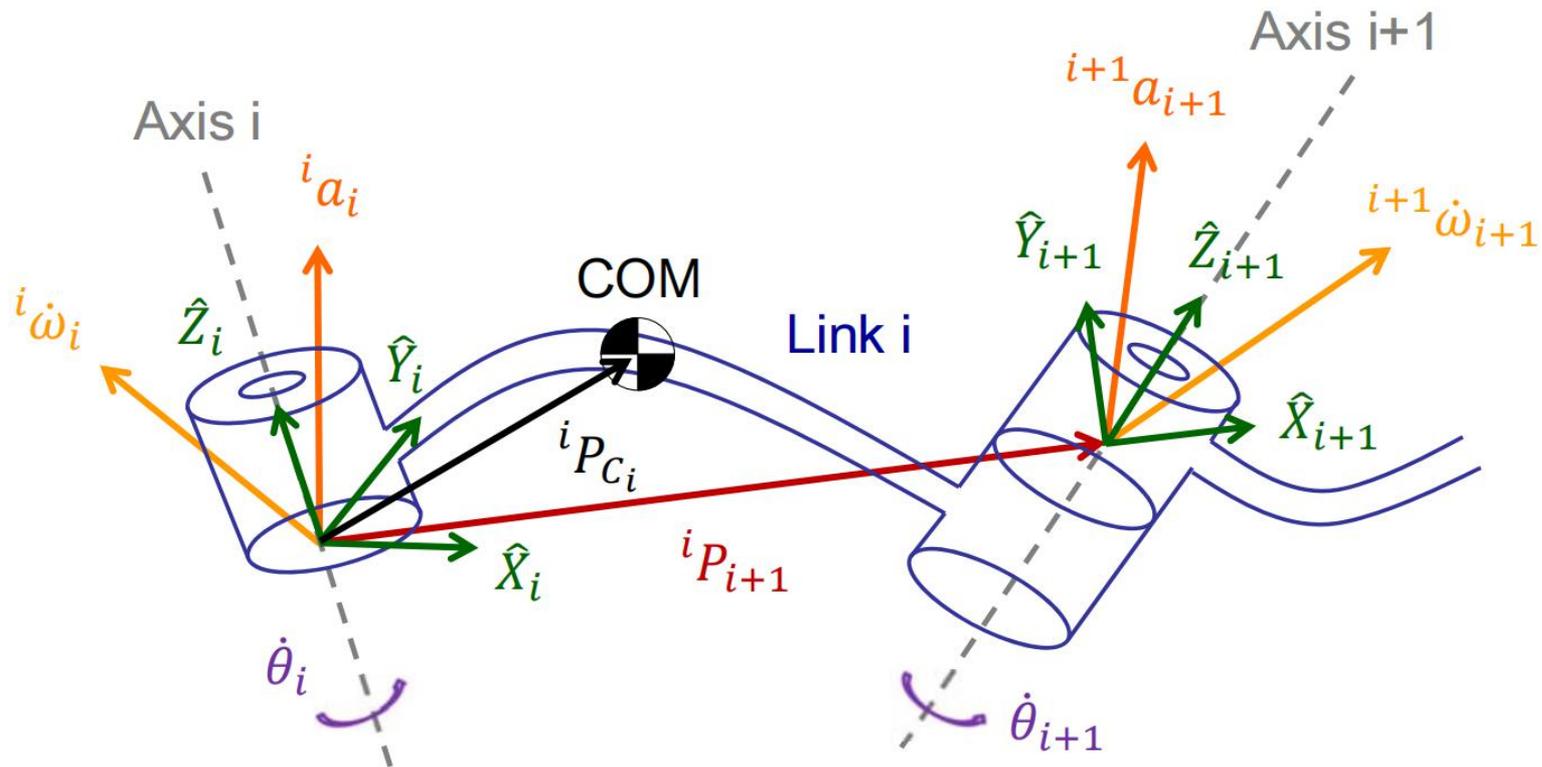
C: 刚体坐标系，原点位于COM

$\underline{C}I$: 常数矩阵



加速度在连杆之间的传递

- 策略：表示坐标系 $\{i\}$ 中连杆 i 的线加速度和角加速度，并找出它们与相邻连杆的线加速度和角加速度的关系





加速度在连杆之间的传递

► 旋转关节 (连杆*i+1*)

◆ 角加速度的传递

在第5章中

$${}^i\omega_{i+1} = {}^i\omega_i + \underbrace{{}^{i+1}R\dot{\theta}_{i+1}}_{} {}^{i+1}\hat{Z}_{i+1}$$

$$\downarrow \text{diff.} \quad \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} = \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_{i+1} \end{bmatrix}$$

$${}^i\dot{\omega}_{i+1} = {}^i\dot{\omega}_i + {}^i\omega_i \times {}^{i+1}R\dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + {}^{i+1}R\ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$

$$\downarrow {}^{i+1}R$$

$${}^{i+i}\dot{\omega}_{i+1} = {}^{i+1}R {}^i\dot{\omega}_i + {}^{i+1}R {}^i\omega_i \times \dot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1} + \ddot{\theta}_{i+1} {}^{i+1}\hat{Z}_{i+1}$$



加速度在连杆之间的传递

◆ 线加速度的传递

$${}^i a_{i+1} = {}^i a_i + {}^i \dot{\omega}_i \times {}^i P_{i+1} + {}^i \omega_i \times ({}^i \omega_i \times {}^i P_{i+1})$$

$$\downarrow {}^{i+1}_i R$$

$${}^{i+1} a_{i+1} = {}^{i+1}_i R ({}^i a_i + {}^i \dot{\omega}_i \times {}^i P_{i+1} + {}^i \omega_i \times ({}^i \omega_i \times {}^i P_{i+1}))$$



加速度在连杆之间的传递

► 平动关节 (连杆*i+1*)

◆ 角加速度的传递

$${}^i\dot{\omega}_{i+1} = {}^i\dot{\omega}_i \xrightarrow{{}^{i+1}_iR} {}^{i+1}\dot{\omega}_{i+1} = {}^{i+1}_iR {}^i\dot{\omega}_i$$

◆ 线加速度的传递

$${}^i a_{i+1} = {}^i a_i + {}^i \dot{\omega}_i \times {}^i P_{i+1} + {}^i \omega_i \times ({}^i \omega_i \times {}^i P_{i+1})$$

$$+ 2 {}^i \omega_i \times {}_{i+1} {}^i R \dot{d}_{i+1} {}^{i+1} \hat{Z}_{i+1} + {}_{i+1} {}^i R \underline{\ddot{d}_{i+1}} {}^{i+1} \hat{Z}_{i+1}$$

$$\downarrow {}^{i+1}_i R \qquad \ddot{d}_{i+1} {}^{i+1} \hat{Z}_{i+1} = {}^{i+1} \begin{bmatrix} 0 \\ 0 \\ \ddot{d}_{i+1} \end{bmatrix}$$

$${}^{i+1} a_{i+1} = {}^{i+1}_i R \left({}^i a_i + {}^i \dot{\omega}_i \times {}^i P_{i+1} + {}^i \omega_i \times ({}^i \omega_i \times {}^i P_{i+1}) \right)$$

$$+ 2 {}^{i+1} \omega_{i+1} \times \dot{d}_{i+1} {}^{i+1} \hat{Z}_{i+1} + \ddot{d}_{i+1} {}^{i+1} \hat{Z}_{i+1}$$



加速度在连杆之间的传递

➤ COM

$${}^i a_{C_i} = {}^i a_i + {}^i \dot{\omega}_i \times {}^i P_{C_i} + {}^i \omega_i \times ({}^i \omega_i \times {}^i P_{C_i})$$

C_i : 第*i*个连杆的COM

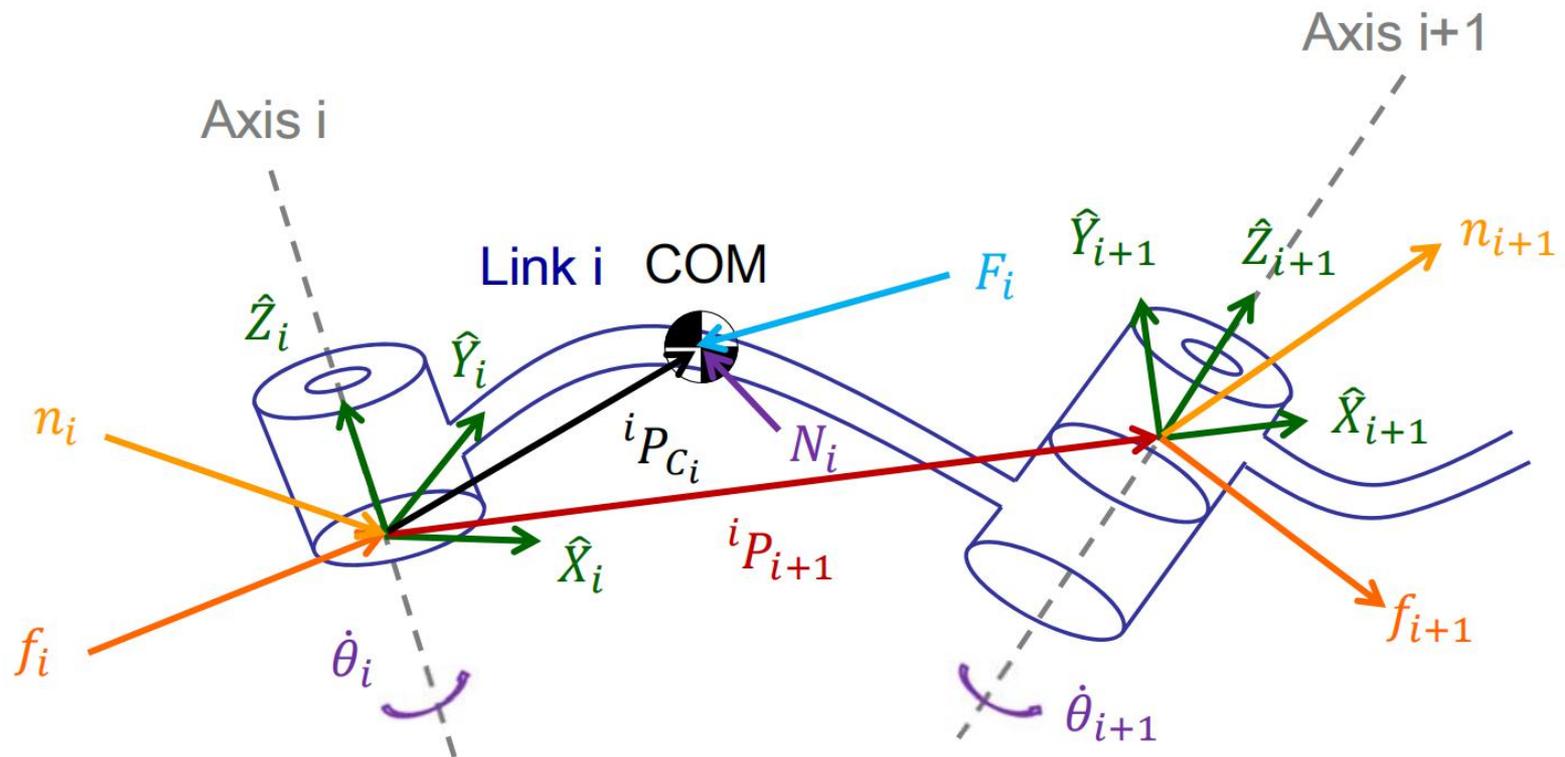


力在连杆之间的传递

► 作用在COM上的惯性力和力矩

$$F_i = ma_{C_i}$$

$$N_i = {}^i C_i I \dot{\omega}_i + \omega_i \times {}^i C_i I \omega_i$$

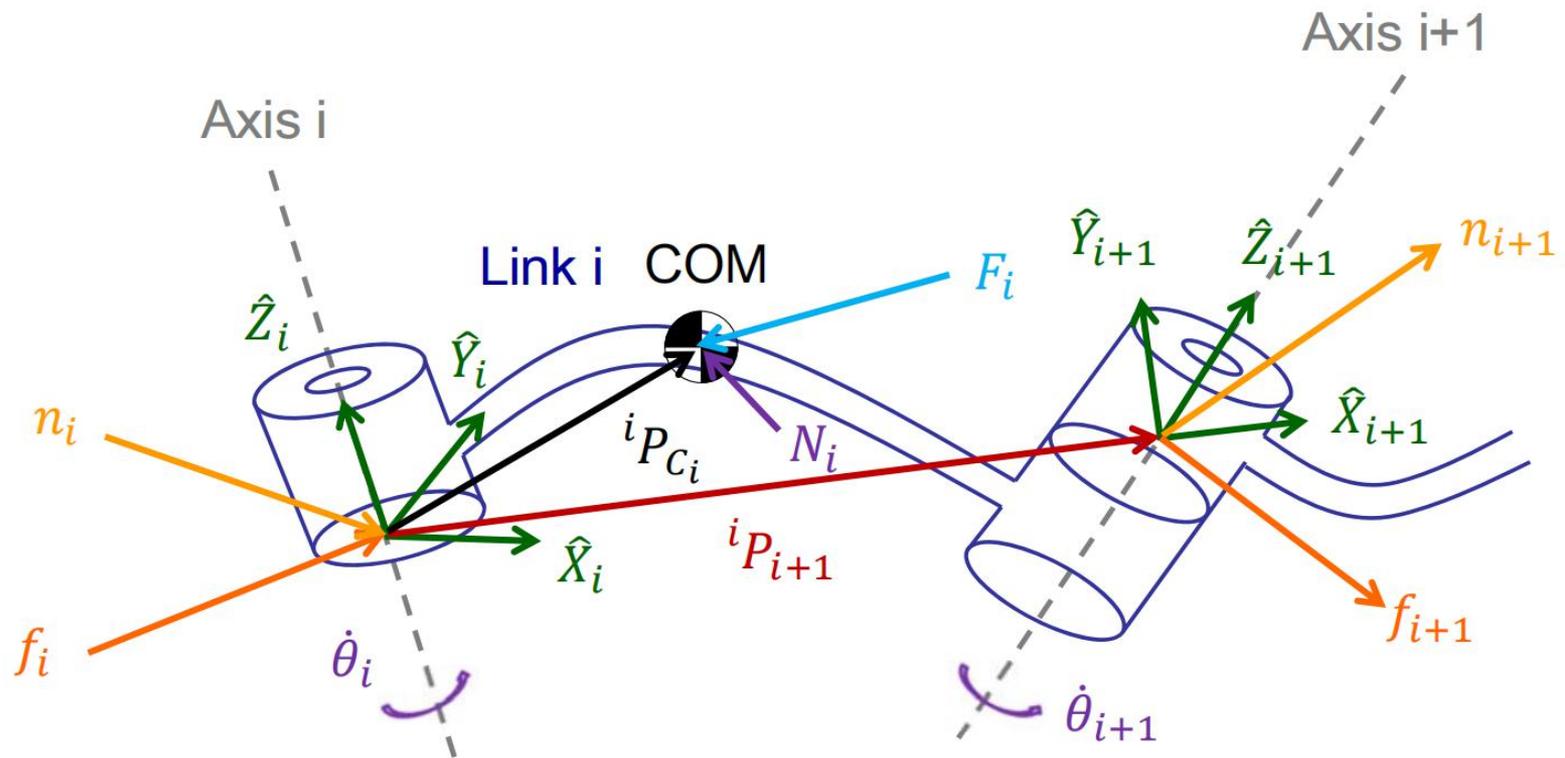




力在连杆之间的传递

$${}^i f_i = {}_{i+1}{}^i R^{i+1} f_{i+1} + {}^i F_i$$

$${}^i n_i = {}_{i+1}{}^i R^{i+1} n_{i+1} + {}^i N_i + {}^i P_{C_i} \times {}^i F_i + {}^i P_{i+1} \times {}_{i+1}{}^i R^{i+1} f_{i+1}$$





力在连杆之间的传递

➤ 因此

◆ 旋转关节

$$\tau_i = {}^i n_i^T {}^i \hat{Z}_i$$

◆ 平动关节

$$\tau_i = {}^i f_i^T {}^i \hat{Z}_i$$

➤ 结论

◆ 包括重力: ${}^0 a_0 = g = 9.81 \text{ m/s}$

◆ 机械臂在自由空间移动 ${}^{N+1} f_{N+1} = 0$ ${}^{N+1} n_{N+1} = 0$



迭代牛顿欧拉动力学方程

➤ 向外迭代

- ◆ 连杆1到连杆n

- ◆ 速度和加速度

➤ 向内迭代

- ◆ 连杆n到连杆1:

- ◆ 力和力矩

- 旋转关节和平动关节：选择正确的方程

- 通用结构，可以应用于任何机械臂

- 方便数字计算



例：一个RR机械臂

➤ 条件

$${}^1P_{C_1} = l_1 \hat{X}_1 \quad c_1 I_1 = 0$$

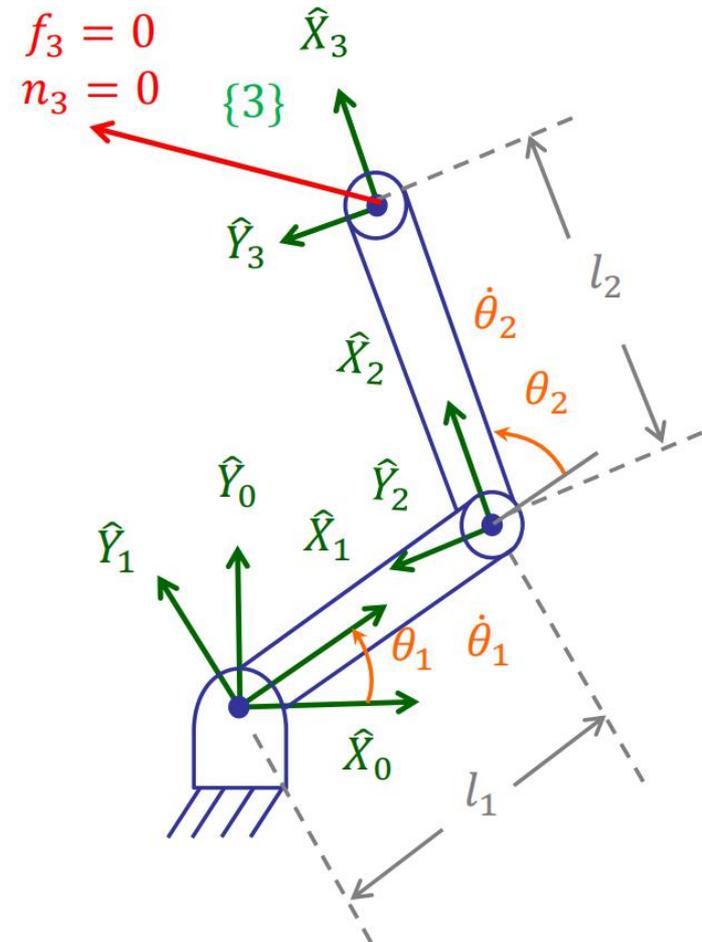
$${}^2P_{C_2} = l_2 \hat{X}_2 \quad c_2 I_2 = 0$$

$$m_1, m_2$$

$$\omega_0 = 0 \quad {}^0v_0 = g \hat{Y}_0$$

$$\dot{\omega}_0 = 0$$

$${}_{i+1}^i R = \begin{bmatrix} c_{i+1} & -s_{i+1} & 0 \\ s_{i+1} & c_{i+1} & 0 \\ 0 & 0 & 1 \end{bmatrix}$$





例：一个RR机械臂

► 速度和加速度的传递

$${}^1\omega_1 = {}^1_0R \cancel{{}^0\omega_0} + \dot{\theta}_1 {}^1\hat{Z}_1 = \dot{\theta}_1 {}^1\hat{Z}_1 = \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_1 \end{bmatrix}$$

$${}^1\dot{\omega}_1 = {}^1_0R \cancel{{}^0\omega_0} + {}^1_0R \cancel{{}^0\omega_0} \times \dot{\theta}_1 {}^1\hat{Z}_1 + \ddot{\theta}_1 \hat{Z}_1 = \begin{bmatrix} 0 \\ 0 \\ \ddot{\theta}_1 \end{bmatrix}$$

$${}^1a_1 = {}^1_0R ({}^0a_0 + \cancel{{}^0\omega_0} \times \cancel{{}^0P_1} + \cancel{{}^0\omega_0} \times (\cancel{{}^0\omega_0} \times \cancel{{}^0P_1})) = \begin{bmatrix} c_1 & s_1 & 0 \\ -s_1 & c_1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ g \end{bmatrix}$$

$${}^1a_{c_1} = {}^1a_1 + {}^1\dot{\omega}_1 \times {}^1P_{c_1} + {}^1\omega_1 \times ({}^1\omega_1 \times {}^1P_{c_1}) = \begin{bmatrix} gs_1 \\ gc_1 \\ 0 \end{bmatrix}$$

$$= \begin{bmatrix} gs_1 \\ gc_1 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ l_1\ddot{\theta}_1 \\ 0 \end{bmatrix} + \begin{bmatrix} -l_1\dot{\theta}_1^2 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} -l_1\dot{\theta}_1^2 + gs_1 \\ l_1\ddot{\theta}_1 + gc_1 \\ 0 \end{bmatrix}$$



例：一个RR机械臂

$${}^1F_1 = m {}^1a_{c_1} \begin{bmatrix} -m_1 l_1 \dot{\theta}_1^2 + m_1 g s_1 \\ m_1 l_1 \ddot{\theta}_1 + m_1 g c_1 \\ 0 \end{bmatrix}$$

$${}^1N_1 = \cancel{c_1 I} {}^1\dot{\omega}_1 + {}^1\omega_1 \times \cancel{c_1 I} {}^1\omega_1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$${}^2\omega_2 = {}^2_1R {}^1\omega_1 + \dot{\theta}_2 {}^2\hat{Z}_2 = \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_1 + \dot{\theta}_2 \end{bmatrix}$$

$${}^2\dot{\omega}_2 = {}^2_1R {}^1\dot{\omega}_1 + {}^2_1R {}^1\omega_1 \times \dot{\theta}_2 {}^2\hat{Z}_2 + \ddot{\theta}_2 {}^2\hat{Z}_2 = \begin{bmatrix} 0 \\ 0 \\ \ddot{\theta}_1 + \ddot{\theta}_2 \end{bmatrix}$$

$$\begin{aligned} {}^2a_2 &= {}^2_1R ({}^1a_1 + {}^1\dot{\omega}_1 \times {}^1P_2 + {}^1\omega_1 \times ({}^1\omega_1 \times {}^1P_2)) = \\ &= \begin{bmatrix} c_2 & s_2 & 0 \\ -s_2 & c_2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} -l_1 \dot{\theta}_1^2 + g s_1 \\ l_1 \ddot{\theta}_1 + g c_1 \\ 0 \end{bmatrix} = \begin{bmatrix} l_1 \ddot{\theta}_1 s_2 - l_1 \dot{\theta}_1^2 c_2 + g s_{12} \\ l_1 \ddot{\theta}_1 c_2 + l_1 \dot{\theta}_1^2 s_2 + g c_{12} \\ 0 \end{bmatrix} \end{aligned}$$



例：一个RR机械臂

$${}^2a_{C_2} = {}^2a_2 + {}^2\dot{\omega}_2 \times {}^2P_{C_2} + {}^2\omega_2 \times ({}^2\omega_2 \times {}^2P_{C_2})$$

$$= \begin{bmatrix} l_1 \ddot{\theta}_1 s_2 - l_1 \dot{\theta}_1^2 c_2 + g s_{12} \\ l_1 \ddot{\theta}_1 c_2 + l_1 \dot{\theta}_1^2 s_2 + g c_{12} \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ l_2 (\ddot{\theta}_1 + \ddot{\theta}_2) \\ 0 \end{bmatrix} + \begin{bmatrix} -l_2 (\dot{\theta}_1 + \dot{\theta}_2)^2 \\ 0 \\ 0 \end{bmatrix}$$

$${}^2F_2 = m {}^2a_{C_2} = \begin{bmatrix} m_2 l_1 \ddot{\theta}_1 s_2 - m_2 l_1 \dot{\theta}_1^2 c_2 + m_2 g s_{12} - m_2 l_2 (\dot{\theta}_1 + \dot{\theta}_2)^2 \\ m_2 l_1 \ddot{\theta}_1 c_2 + m_2 l_1 \dot{\theta}_1^2 s_2 + m_2 g c_{12} + m_2 l_2 (\ddot{\theta}_1 + \ddot{\theta}_2) \\ 0 \end{bmatrix}$$

$${}^2N_2 = {}^{C_2}I {}^2\dot{\omega}_2 + {}^2\omega_2 \times {}^{C_2}I {}^2\omega_2 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$



例：一个RR机械臂

► 力和力矩的传递

$${}^2f_2 = {}^2_3R {}^3f_3 + {}^2F_2 = {}^2F_2$$

$${}^2n_2 = {}^2_3R {}^3n_3 + {}^2N_2 + {}^2P_{C_2} \times {}^2F_2 + {}^2P_3 \times {}^2_3R {}^3f_3$$

$$= \begin{bmatrix} 0 \\ 0 \\ m_2 l_1 l_2 c_2 \ddot{\theta}_1 + m_2 l_1 l_2 s_2 \dot{\theta}_1^2 + m_2 l_2 g c_{12} + m_2 l_2^2 (\ddot{\theta}_1 + \ddot{\theta}_2) \end{bmatrix}$$

$${}^1f_1 = {}^1_2R {}^2f_2 + {}^1F_1$$

$$= \begin{bmatrix} c_2 & -s_2 & 0 \\ s_2 & c_2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} m_2 l_1 s_2 \ddot{\theta}_1 - m_2 l_1 c_2 \dot{\theta}_1^2 + m_2 g s_{12} - m_2 l_2 (\dot{\theta}_1 + \dot{\theta}_2)^2 \\ m_2 l_1 c_2 \ddot{\theta}_1 + m_2 l_1 s_2 \dot{\theta}_1^2 + m_2 g c_{12} + m_2 l_2 (\ddot{\theta}_1 + \ddot{\theta}_2) \\ 0 \end{bmatrix}$$

$$+ \begin{bmatrix} -m_1 l_1 \dot{\theta}_1^2 + m_1 g s_1 \\ m_1 l_1 \ddot{\theta}_1 + m_1 g c_1 \\ 0 \end{bmatrix}$$



例：一个RR机械臂

$$\begin{aligned} {}^1n_1 &= {}^1_2R {}^2n_2 + {}^1N_1 + {}^1P_{C_1} \times {}^1F_1 + {}^1P_2 \times {}^1_2R {}^2f_2 \\ &= \begin{bmatrix} 0 \\ 0 \\ m_2l_1l_2c_2\ddot{\theta}_1 + m_2l_1l_2s_2\dot{\theta}_1^2 + m_2l_2gc_{12} + m_2l_2^2(\ddot{\theta}_1 + \ddot{\theta}_2) \end{bmatrix} \\ &\quad + \begin{bmatrix} 0 \\ 0 \\ m_1l_1^2\ddot{\theta}_1 + m_1l_1gc_1 \end{bmatrix} \\ &\quad + \begin{bmatrix} 0 \\ 0 \\ m_2l_1^2\ddot{\theta}_1 - m_2l_1l_2s_2(\dot{\theta}_1 + \dot{\theta}_2)^2 + m_2l_1gs_2s_{12} + m_2l_1l_2c_2(\ddot{\theta}_1 + \ddot{\theta}_2) + m_2l_1gc_2c_{12} \end{bmatrix} \end{aligned}$$



例：一个RR机械臂

► 关节力矩

$$\begin{aligned}\tau_1 &= {}^1n_1^T {}^1\widehat{Z}_1 \\ &= m_2 l_2^2 (\ddot{\theta}_1 + \ddot{\theta}_2) + m_2 l_1 l_2 c_2 (2\ddot{\theta}_1 + \ddot{\theta}_2) + (m_1 + m_2) l_1^2 \ddot{\theta}_1 \\ &\quad - m_2 l_1 l_2 s_2 \dot{\theta}_2^2 - 2m_2 l_1 l_2 s_2 \dot{\theta}_1 \dot{\theta}_2 + m_2 l_2 g c_{12} + (m_1 + m_2) l_1 g c_1\end{aligned}$$

$$\begin{aligned}\tau_2 &= {}^2n_2^T {}^2\widehat{Z}_2 \\ &= m_2 l_1 l_2 c_2 \ddot{\theta}_1 + m_2 l_1 l_2 s_2 \dot{\theta}_1^2 + m_2 l_2 g c_{12} + m_2 l_2^2 (\ddot{\theta}_1 + \ddot{\theta}_2)\end{aligned}$$



动力学方程的结构

➤ 状态空间方程

$$\tau = M(\Theta)\ddot{\Theta} + V(\Theta, \dot{\Theta}) + G(\Theta)$$

$n \times 1$ $n \times n$ $n \times 1$ $n \times 1$ $n \times 1$

质量矩阵 离心力和
科氏力矩
阵 重力矩阵

➤ 回顾RR机械臂

$$M(\Theta) = \begin{bmatrix} l_2^2 m_2 + 2l_1 l_2 m_2 c_2 + l_1^2 (m_1 + m_2) & l_2^2 m_2 + l_1 l_2 m_2 c_2 \\ l_2^2 m_2 + l_1 l_2 m_2 c_2 & l_2^2 m_2 \end{bmatrix}$$

$$V(\Theta, \dot{\Theta}) = \begin{bmatrix} -m_2 l_1 l_2 s_2 \dot{\theta}_2^2 - 2m_2 l_1 l_2 s_2 \dot{\theta}_1 \dot{\theta}_2 \\ m_2 l_1 l_2 s_2 \dot{\theta}_1^2 \end{bmatrix}$$

$$G(\Theta) = \begin{bmatrix} m_2 l_2 g c_{12} + (m_1 + m_2) l_1 g c_1 \\ m_2 l_2 g c_{12} \end{bmatrix}$$



动力学方程的结构

► 位形空间方程

$$\tau = M(\Theta)\ddot{\Theta} + B(\Theta)[\dot{\Theta}\dot{\Theta}] + C(\Theta)[\dot{\Theta}^2] + G(\Theta)$$

$n \times 1$ $n \times n$ $n \times \frac{n(n-1)}{2}$ $n \times n$ $n \times 1$
 质量矩阵 科氏力矩阵 离心力矩阵 重力矩阵

$$[\dot{\Theta}\dot{\Theta}] = [\dot{\theta}_1\dot{\theta}_2 \quad \dot{\theta}_1\dot{\theta}_3 \quad \dots \quad \dot{\theta}_{n-1}\dot{\theta}_n]^T$$

$$\frac{n(n-1)}{2} \times 1$$

$$[\dot{\Theta}^2] = [\dot{\theta}_1^2 \quad \dot{\theta}_2^2 \quad \dots \quad \dot{\theta}_n^2]^T$$

$$n \times 1$$



动力学方程的结构

➤ 回顾RR机械臂

$$V(\Theta, \dot{\Theta}) = \begin{bmatrix} -m_2 l_1 l_2 s_2 \dot{\theta}_2^2 - 2m_2 l_1 l_2 s_2 \dot{\theta}_1 \dot{\theta}_2 \\ m_2 l_1 l_2 s_2 \dot{\theta}_1^2 \end{bmatrix} = B(\Theta) [\dot{\Theta} \dot{\Theta}] + C(\Theta) [\dot{\Theta}^2]$$

$$B(\Theta) = \begin{bmatrix} -2m_2 l_1 l_2 s_2 \\ 0 \end{bmatrix} \quad [\dot{\Theta} \dot{\Theta}] = [\dot{\theta}_1 \dot{\theta}_2]$$

$$C(\Theta) = \begin{bmatrix} 0 & -m_2 l_1 l_2 s_2 \\ m_2 l_1 l_2 s_2 & 0 \end{bmatrix} \quad [\dot{\Theta}^2] = \begin{bmatrix} \dot{\theta}_1^2 \\ \dot{\theta}_2^2 \end{bmatrix}$$



机械臂动力学的拉格朗日方程

- ▶ 牛顿-欧拉法：基于力和力矩的分析
- ▶ 拉格朗日：基于能量的分析
- ▶ 对于一个系统来说，两种方法应该得到同样的运动方程



机械臂动力学的拉格朗日方程

► 动能

$$k_i = \frac{1}{2} m_i v_{c_i}^T v_{c_i} + \frac{1}{2} {}^i \omega_i^T C_i I_i {}^i \omega_i$$

$$k = \sum_{i=1}^n k_i \quad k = k(\Theta, \dot{\Theta}) = \frac{1}{2} \dot{\Theta}^T M(\Theta) \dot{\Theta}$$

► 势能 (位能)

$$u_i = -m_i {}^0 g^T {}^0 P_{c_i} + \underline{u_{ref_i}}$$

Shift the zero reference height

$$u = \sum_{i=1}^n u_i \quad u = u(\Theta)$$



➤ 拉格朗日

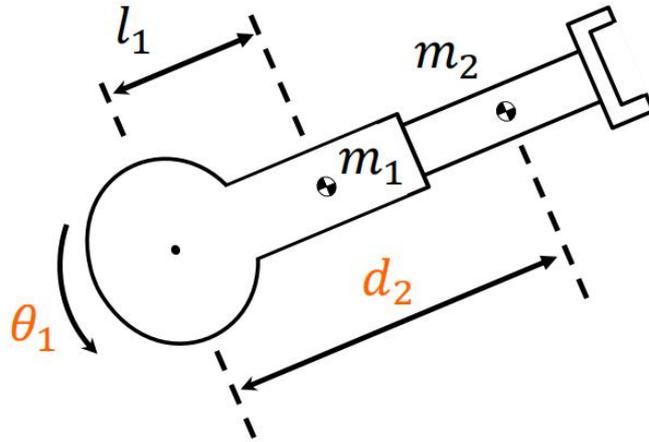
$$\mathcal{L}(\Theta, \dot{\Theta}) = k(\Theta, \dot{\Theta}) - u(\Theta)$$

➤ 机械臂的运动方程

$$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{\Theta}} - \frac{\partial \mathcal{L}}{\partial \Theta} = \tau$$

$$\frac{d}{dt} \frac{\partial k}{\partial \dot{\Theta}} - \frac{\partial k}{\partial \Theta} + \frac{\partial u}{\partial \Theta} = \tau$$

例：一个RP机械臂



$${}^{c_1}I_1 = \begin{bmatrix} I_{xx1} & 0 & 0 \\ 0 & I_{yy1} & 0 \\ 0 & 0 & I_{zz1} \end{bmatrix}$$

$${}^{c_2}I_2 = \begin{bmatrix} I_{xx2} & 0 & 0 \\ 0 & I_{yy2} & 0 \\ 0 & 0 & I_{zz2} \end{bmatrix}$$

➤ 动能

$$k_1 = \frac{1}{2} m_1 l_1^2 \dot{\theta}_1^2 + \frac{1}{2} I_{zz1} \dot{\theta}_1^2$$

$$k_2 = \frac{1}{2} m_2 (d_2^2 \dot{\theta}_1^2 + \dot{d}_2^2) + \frac{1}{2} I_{zz2} \dot{\theta}_1^2$$

$$k(\Theta, \dot{\Theta}) = \frac{1}{2} (m_1 l_1^2 + I_{zz1} + I_{zz2} + m_2 d_2^2) \dot{\theta}_1^2 + \frac{1}{2} m_2 \dot{d}_2^2$$



例：一个RP机械臂

➤ 势能

$$u_1 = m_1 g l_1 \sin \theta_1 + m_1 g l_1$$

$$u_2 = m_2 g d_2 \sin \theta_1 + m_2 g d_{2max}$$

$$u(\Theta) = (m_1 l_1 + m_2 d_2) g \sin \theta_1 + \underline{m_1 g l_1 + m_2 g d_{2max}}$$

Shift the zero reference height

➤ 拉格朗日

$$\frac{\partial k}{\partial \dot{\Theta}} = \begin{bmatrix} (m_1 l_1^2 + I_{zz1} + I_{zz2} + m_2 d_2^2) \dot{\theta}_1 \\ m_2 \dot{d}_2 \end{bmatrix}$$

$$\frac{\partial k}{\partial \Theta} = \begin{bmatrix} 0 \\ m_2 d_2 \dot{\theta}_1^2 \end{bmatrix}$$

$$\frac{\partial u}{\partial \Theta} = \begin{bmatrix} (m_1 l_1 + m_2 d_2) g \cos \theta_1 \\ m_2 g \sin \theta_1 \end{bmatrix}$$



例：一个RP机械臂

➤ 运动方程

$$\tau_1 = (m_1 l_1^2 + I_{zz1} + I_{zz2} + m_2 d_2^2) \ddot{\theta}_1 + 2m_2 d_2 \dot{\theta}_1 \dot{d}_2 + (m_1 l_1 + m_2 d_2) g \cos \theta_1$$

$$\tau_2 = m_2 \ddot{d}_2 - m_2 d_2 \dot{\theta}_1^2 + m_2 g \sin \theta_1$$

➤ 状态空间表达

$$\tau = M(\Theta) \ddot{\Theta} + V(\Theta, \dot{\Theta}) + G(\Theta)$$

$$M(\Theta) = \begin{bmatrix} m_1 l_1^2 + I_{zz1} + I_{zz2} + m_2 d_2^2 & 0 \\ 0 & m_2 \end{bmatrix}$$

$$V(\Theta, \dot{\Theta}) = \begin{bmatrix} 2m_2 d_2 \dot{\theta}_1 \dot{d}_2 \\ -m_2 d_2 \dot{\theta}_1^2 \end{bmatrix}$$

$$G(\Theta) = \begin{bmatrix} (m_1 l_1 + m_2 d_2) g \cos \theta_1 \\ m_2 g \sin \theta_1 \end{bmatrix}$$



➤ 动态方程

◆ 关节空间

$$\tau = M(\theta)\ddot{\theta} + V(\theta, \dot{\theta}) + G(\theta)$$

◆ 笛卡尔空间

$$F = M_x(\theta)\ddot{X} + V_x(\theta, \dot{\theta}) + G_x(\theta)$$

➤ 方程

$$\tau = J^T(\theta)F$$

$$F = J^{-T}\tau = J^{-T}M(\theta)\ddot{\theta} + J^{-T}V(\theta, \dot{\theta}) + J^{-T}G(\theta)$$

$$\dot{X} = J\dot{\theta} \quad \ddot{X} = j\dot{\theta} + J\ddot{\theta} \quad \ddot{\theta} = J^{-1}\ddot{X} - J^{-1}j\dot{\theta}$$



笛卡尔空间中的机械臂动力学

$$\begin{aligned} F &= J^{-T} M(\Theta) J^{-1} \ddot{X} - J^{-T} M(\Theta) J^{-1} \dot{j} \dot{\Theta} + J^{-T} V(\Theta, \dot{\Theta}) + J^{-T} G(\Theta) \\ &= M_x(\Theta) \ddot{X} + V_x(\Theta, \dot{\Theta}) + G_x(\Theta) \end{aligned}$$

$$M_x(\Theta) = J^{-T}(\Theta) M(\Theta) J^{-1}(\Theta)$$

$$V_x(\Theta, \dot{\Theta}) = J^{-T}(\Theta) (V(\Theta, \dot{\Theta}) - M(\Theta) J^{-1}(\Theta) \dot{j}(\Theta) \dot{\Theta})$$

$$G_x(\Theta) = J^{-T}(\Theta) G(\Theta)$$



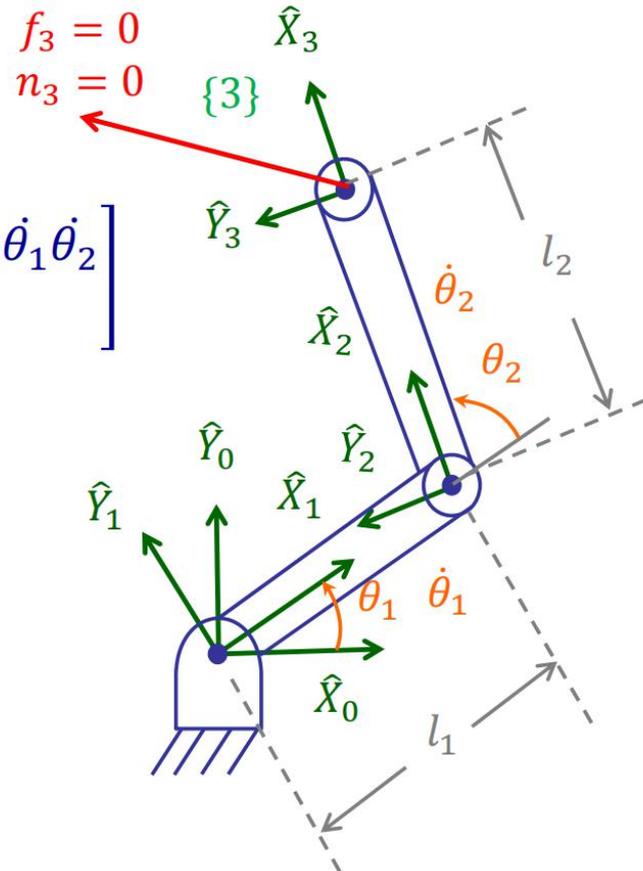
回顾例：一个RP机械臂

► 关节空间

$$M(\Theta) = \begin{bmatrix} l_2^2 m_2 + 2l_1 l_2 m_2 c_2 + l_1^2 (m_1 + m_2) & l_2^2 m_2 + l_1 l_2 m_2 c_2 \\ l_2^2 m_2 + l_1 l_2 m_2 c_2 & l_2^2 m_2 \end{bmatrix}$$

$$V(\Theta, \dot{\Theta}) = \begin{bmatrix} -m_2 l_1 l_2 s_2 \dot{\theta}_2^2 - 2m_2 l_1 l_2 s_2 \dot{\theta}_1 \dot{\theta}_2 \\ m_2 l_1 l_2 s_2 \dot{\theta}_1^2 \end{bmatrix}$$

$$G(\Theta) = \begin{bmatrix} m_2 l_2 g c_{12} + (m_1 + m_2) l_1 g c_1 \\ m_2 l_2 g c_{12} \end{bmatrix}$$





回顾例：一个RP机械臂

➤ 雅可比矩阵

$$J(\Theta) = \begin{bmatrix} l_1 s_2 & 0 \\ l_1 c_2 + l_2 & l_2 \end{bmatrix} \quad J^{-1}(\Theta) = \frac{1}{l_1 l_2 s_2} \begin{bmatrix} l_2 & 0 \\ -l_1 c_2 - l_2 & l_1 s_2 \end{bmatrix}$$

$$j(\Theta) = \begin{bmatrix} l_1 c_2 \dot{\theta}_2 & 0 \\ -l_1 s_2 \dot{\theta}_2 & 0 \end{bmatrix}$$

➤ 笛卡尔空间

$$M_x(\Theta) = J^{-T}(\Theta) M(\Theta) J^{-1}(\Theta) = \begin{bmatrix} m_2 + \frac{m_1}{s_2^2} & 0 \\ 0 & m_2 \end{bmatrix}$$

$$V_x(\Theta, \dot{\Theta}) = J^{-T}(\Theta) (V(\Theta, \dot{\Theta}) - M(\Theta) J^{-1}(\Theta) j(\Theta) \dot{\Theta})$$

$$= \begin{bmatrix} -(m_2 l_1 c_2 + m_2 l_2) \dot{\theta}_1^2 - m_2 l_2 \dot{\theta}_2^2 - (2m_2 l_2 + m_2 l_1 c_2 + m_1 l_1 \frac{c_2}{s_2^2}) \dot{\theta}_1 \dot{\theta}_2 \\ m_2 l_1 s_2 \dot{\theta}_1^2 + m_2 l_1 s_2 \dot{\theta}_1 \dot{\theta}_2 \end{bmatrix}$$

$$G_x(\Theta) = J^{-T}(\Theta) G(\Theta) = \begin{bmatrix} m_1 g \frac{c_1}{s_2} + m_2 g s_{12} \\ m_2 g c_{12} \end{bmatrix}$$



➤ 笛卡尔空间

$$\tau = J^T(\Theta)F = J^T(\Theta)(M_x(\Theta)\ddot{X} + V_x(\Theta, \dot{\Theta}) + G_x(\Theta))$$

$$\tau = J^T(\Theta)M_x(\Theta)\ddot{X} + B_x(\Theta)[\dot{\Theta}\dot{\Theta}] + C_x(\Theta)[\dot{\Theta}^2] + G(\Theta)$$

$$\Rightarrow J^T(\Theta)V_x(\Theta, \dot{\Theta}) = B_x(\Theta)[\dot{\Theta}\dot{\Theta}] + C_x(\Theta)[\dot{\Theta}^2]$$



回顾例：一个RP机械臂

$$J^T(\Theta)V_x(\Theta, \dot{\Theta}) = B_x(\Theta)[\dot{\Theta}\dot{\Theta}] + C_x(\Theta)[\dot{\Theta}^2]$$

$$= \begin{bmatrix} l_1 s_2 & l_1 c_2 + l_2 \\ 0 & l_2 \end{bmatrix} \begin{bmatrix} -(m_2 l_1 c_2 + m_2 l_2) \dot{\theta}_1^2 - m_2 l_2 \dot{\theta}_2^2 - (2m_2 l_2 + m_2 l_1 c_2 + m_1 l_1 \frac{c_2}{s_2^2}) \dot{\theta}_1 \dot{\theta}_2 \\ m_2 l_1 s_2 \dot{\theta}_1^2 + l_1 m_2 s_2 \dot{\theta}_1 \dot{\theta}_2 \end{bmatrix}$$

$$B_x(\Theta) = \begin{bmatrix} -m_1 l_1^2 \frac{c_2}{s_2} - m_2 l_1 l_2 s_2 \\ m_2 l_1 l_2 s_2 \end{bmatrix}$$

$$C_x(\Theta) = \begin{bmatrix} 0 & -m_2 l_1 l_2 s_2 \\ m_2 l_1 l_2 s_2 & 0 \end{bmatrix}$$



➤ 粘性摩擦

$$\tau_{friction} = c\dot{\theta}$$

➤ 库伦摩擦

$$\tau_{friction} = c \operatorname{sgn}\dot{\theta}$$

$\dot{\theta} = 0, c = \text{“static coefficient”}$

$\dot{\theta} \neq 0, c = \text{“dynamic coefficient”}$



谢谢!

